

VIC Matrix Circuit

Instant Explosion of Water

VIC Coil Assembly is specially designed to allow Voltage Potential of "opposite electrical attraction force" of High Voltage Intensity" to "instantly" release Thermal Explosive Energy (gtnt) from natural water.

The Voltage Intensifier Circuit takes advantage of the "Electron Bounce Phenomenon" to trigger Hydrogen Fracturing Process without amp influxing.

Interlinked with VIC Coil Assembly, the Water Fuel Injector acts and performs as a "Voltage Amplifier" by simply altering the Voltage Wave Guide to either form a "compressional" or "Expanded" Voltage Wave Form that increases Electrical Voltage intensity beyond applied excitation voltage outputted from VIC Coil.

The "Mode of Operability" of VIC Coil Assembly is systematically -activated by a programmable signal input, and is performed in the following way:

Section 7

VIC Matrix Circuit

Instant Explosion of
Water

The "mode-of-operability" of VIC Coil Assembly allows Voltage Potential of opposite voltage polarity to increase and be attenuated up to and beyond 20 Kilovolts while inhibiting and restricting amp leakage in the milliamperes range ... establishing operational parameter of utilizing "Opposite Electrical Attraction Force" of "high voltage intensity" to "instantly" releases thermal explosive energy (gnt) from natural water. The Voltage Intensifier Circuit takes advantage of the "Electron Bounce Phenomenon" to trigger Hydrogen Fracturing Process without amp influxing. Taper Resonant Cavity functions as a "Voltage Amplifier" when interlinked with VIC Circuit.

Voltage Intensifier Circuit (60) of Figure (3-22) (Memo WFC 422 DA) as to Figure (1-1) (Memo WFC 420) and Voltage Intensifier Circuit (620) of Figure (7-1) are specifically designed to restrict amp flow during Programmable Pulsing Operations (49a xxx 49n) but in different operational modes: VIC voltage circuit (60) utilizes copper wire-wrap to form Resonant Charging Chokes (56/62) of Figure (3-22) in conjunction with Switching Diode (55) to encourage and make use of "Electron Bounce" phenomena (700) of Figure (7-9) to help promote Step Charging Effect (628) of Figure (7-7) by preventing electrical discharge of Resonant Cavity (140 - 170) since Blocking Diode functions as an "Open" switch during Pulse Off-time; whereas, VIC Voltage Enhancement Circuit (VIC - VB) (620) of Figure (7-1) incorporates the use of stainless steel wire-wrap coils (614/615) to accomplish the formation of unipolar gated pulse-wave (64a xxx T3 xxx 64n) without experiencing "signal distortion" or "signal degradation" (preventing transformer ringing during signal propagation) as elevated voltage levels (- xx Vc- xx Vd - xx Vn) while allowing the reduction of Capacitor-Gap (Cp) (616) of Figure (7-11) width spacing (57 of Figure 3-25 ~35 of Figure 6-2) (typically .060 - .010) respectively. as illustrated in Tubular Resonant Cavity (170) as to Taper Resonant Cavity (620) of Figure (7-1).

Switching Diode (55) of Figure (3-22) prevents Bidirectional electron flow (current flow in one direction only) since Blocking - Diode (55) only conducts "current flow" in the direction of schematic-arrow while being placed in-line with VIC Circuit impedance interaction ($R1 + Z2 + Z3 \cdot Re$), as mathematically extrapolated in Circuit Equation (Eq 9) ... Diode (55) being placed between Secondary Pickup Coil (52) and Resonant Charging Choke (56) to act as an electronic switch in open-position during pulse off-time (T2) of Figure (7-8) while preventing electron flow

in reverse direction when Inductor (L1) collapsing electromagnetic field (FL1) produces another unipolar pulse wave-form (64a - 64b) ... producing unipolar voltage wave-form (64a xxx 64n) during repeated pulse-signal (46a xxx 46n) on-time (T1a xxx T1n) ... allowing the formation of an gated pulse- frequency pulse-train (64a/64b - T3 - 64a/64b) when pulse off-time (T3) is greater than time-period (T2) ... input-signal (49a xxx 49n) being a Pulse-Train where (T2) pulse offtime (T2) is adjusted to allows Unipolar Pulse-Train (64a xxx T3 xxx 64n) ... outputting Voltage-wave signal (64a xxx 64n) being a pulse-frequency doubler due to Inductance Reactance (FL) of Inductor Coil (56) of Figure (3-22) when collapsing magnetic field (FI) of Figure (7-3b) re-cuts coil-wrap (LI) during each pulse off-time (T2) ... producing a second unipolar voltage wave-form (64b) during the rise and fall of magnetic field (71), as further illustrated in (620) of Figure (7-1).

Resistance (Rs)

In reference to the use stainless steel (s/s) coil-wrap (614/615), resistive wire value (Rsl/Rs2) of Figure (7-8) (typically 11.6K ohms per coil) is sufficient enough to inhibit current flow oscillation in direct relationship to circuit impedance (Eq. 9) since "current flow" is, also, restricted in the milliamper (s) range due to (s/s) wire material (Rsl/Rs2) composition ability to oppose electron interaction or electron interchange from one atomic structure to another; while, at the same time, conducting and permitting the transmission of "Voltage Potential" across circumference surface area (skin effect) (66/67) of Figure (7-11) as to Figure (590) of Figure (6-2) to bring-on and perform Voltage Wave-Guide phenomena (57) of Figure (6-2) ... causing and allowing the applied Electrical Stress of opposite voltage polarity (ST-ST' - RU-RU') to trigger Hydrogen Fracturing Process (390) of Figure (3-42) in an instant of time ... releasing thermal explosive energy (gtnt) (16) of Figure (4-5) on demand from natural water (85) of Figure (3-26) since the dielectric value (Re) of (Eq.9) of Water Fuel (85) is further approximated in Capacitance Equation (Eq.22), as illustrated in (650) of Figure (7-4) as to Tapered Voltage Wave-Guide (720) of Figure (7-11) ... allowing the dielectric value of Water (Re) to be a part of Voltage Intensifier Circuit (110) of Figure (4-9) capability of restricting amp flow during Voltage Pulsing Operation (49a xxx 49n) of (620) of Figure (7-1) as to VIC Matrix Circuit (690) of Figure (7-8) ... allowing applied opposite Voltage potential (ST-ST' - RU-RU') to perform work without amp "influxing", as systematically depicted in VIC Matrix Circuit (690) below.

Inductance (FL)

Component Interaction promotes Component Reactance during D.C. pulsing operations

while allowing variable voltage amplitude ($V_o - V_a - V_b - V_n$) of Figure (7-13) to be attenuated independently of Voltage Pulse frequency (49a xxx 49n), as so illustrated in (600) of Figure (6-3).

Resonant Charging Circuit (630) of Figure (7-2) being an LC Circuit is fanned when Inductor (614) of Figure (7-1) is electrically linked to Taper Capacitor (720) of Figure (7-11) in series arrangement. Inductor (614) is an insulated wire wound in a spiral pathway around Bobbin Cavity (580) of Figure (6-1) to form Voltage Stepping Coil (710) of Figure (7-10) as to (580) of Figure (6-1). Capacitor (E9/E10) of figure (6-2) as to (720) of Figure (7-11) is formed when outer tapered surface (66) and inner tapered surface (67) forms Water-Gap (616) of Figure (7-11) as to Figure (590) of Figure (6-2) having placed there between Dielectric Water Bath (85/Re), as schematically illustrated in matrix outline in (670) of Figure (7-6) as to (690) of Figure (7-8) and further detailed in Electrical Charging Effect (650) of Figure (7-4).

Component Reactance to D.C. pulsing transforms inductor (614) of Figure (7-1) / Capacitor (E9/E10) of Figure (7-11) LC circuit of Figure (7-2) into an Resonant Charging Choke (614) which steps up an unipolar oscillation of an given charging frequency with the effective capacitance of an pulse-forming network (64a xxx 64n) of Figure (7-1) as to (600) of Figure (6-3) in order to charge Voltage Zones (E9/E10) to an higher potential beyond applied voltage input ... interacting Distributed Capacitance (C_{da} xxx C_{dn}) and Distributed Inductance (D_{Ia} xxx D_{In}) of Figure (7-3) of Inductor Coil (614) of (7-1) with "Electrical Charging Effect" brought on by the dielectric value of water bath (85/Re), as pictorially illustrated in (650) of Figure (7-4). The established Dielectric Value of Water (85) being 78.54 ohms since the electron "L" orbit of the water molecule (210) of Figure (3-27) occupies the maximum allowable number of eight electrons when covalent linkup of 'unlike oxygen atom (76) and hydrogen atoms (77a/b) occurs "' . ' stabilizing Water molecule (85) into existence ... thereby, maintaining molecular stability of water by opposing the exchange of electrons from an external electron source (amp inducing circuit) beyond molecular Structure (85). Electron interaction (movement of electrons through the liquid medium of water) is further inhibited since natural water contaminates (144a xxx 144n) of Figure (3-24) is normally less than 20 ppm ... distilled water, of course, is generally lab-tested Ippm or less, as illustrated in (760) of Figure (7-15) as to (750) of Figure (7-14).

Capacitance (Cd)

. Capacitor (E9/E10) of Figure (7-1) as to Figure (650) of Figure (7-4) in direct relationship to Water Gap (616) becomes Taper Resonant Cavity (720) of Figure (7-11) as shown in (590) of

Figure (6-2) since Water Gap (616) is occupied by a dielectric liquid (Re) as herein before identified as natural water (85) having no electrolyte added thereto ... generally rain water (85f) (750) of Figure (7-14) being almost free of contaminates due to Water Evaporation Process (532) of Figure (5-6) ... rain water (850) being an liquid-insulator that restricts the flow of amps ... a resistive liquid (having an ohmic value of 78.54 ohms) that takes on an "Electrical Charge" when applied voltage Potential (66/67) of Figure (7-1) as to (650) of Figure (7-4) causes and sets up Molecular Polarization Alinement (617) of Figure (7-4) by way of electrical molecular rotation (opposite electrical attraction force to rotate and position particle alinement) of each water Molecule (85a - 85b - 85c - 85n). being subjected to opposite electrical attraction forces (SS' - RR '). In like manner, the stainless steel (s/s) TiO4 material that forms Voltage Zones (E9/EI0) undergo particle alinement of its atomic structure within the atomic infrastructure of plate-material (E9/E 10) when exposed to the same applied electrical voltage fields (66/67) after a pre-set time ... causing molecular electrical movement to occur within the surface-material (E9/EI0) ... which, after occurring, the newly formed molecular electrical orientation (625a xxx 625n) of Figure (7-4) remains in electrical atomic alinement after pulse off-time (T2). aiding the transference of voltage potential during pulse on-time (T1).. allowing the resultant Surface Polarity Effect (skin effect) (624) of Figure (7-7) to supply a sufficient residual atomic "Electrical Charge Field" to help maintain molecular alinement of water atoms (617) during pulsing operations, as illustrated in (680) of Figure (7-7). Inherently, then, Resonant Cavity (720) of Figure (7-11) as to (650) of Figure (7-4) forms capacitor (ER) of Figure (7-1) when the dielectric liquid of water (85) is placed or injected between electrical conducting plates (E9/EI0) while applied voltage Potential of opposite polarity (66/67) is directly exposed to Water Molecules (85a xxx 85n), as depicted in Taper Resonant Cavity (590) of Figure (6.;2) as to (650) of Figure (7-4).

Inductor (614) and Inductor (615) of Figure (7-1) as to (670) of Figure (7-6) is wound or coil-wrapped (see multi-layer equation Eq. 20) in such a manner as to increase the magnetic flux intensity (DIa xxx DIIn) of Figure (7-3) as to (580) as to Figure (6-1) in reference to (710) of Figure (7-10) between the turns (618a xxx 618n) of coil-wrap (640). The circular-spiral turns of wire (forming parallel electrical surfaces) is separated by an Insulated Dielectric Coating Material which forms a series of capacitors (Cda xxx Cdn) when magnetic flux-lines (619a xxx 619n) produces Electromagnetic Coupling Field (621) during pulse on-time (T1), as illustrated in (640) of Figure (7-3) as to (690) of Figure (7-8). The series resistance value (Rs) in (670) of Figure (.76) as to (690) of Figure (7-8) and (670) of Figure (7-6) is determined by ρ composition of the wire material in terms of its ohmic value (electrical resistivity) per given length and diameter cross-section: Resonant Charging Chokes (614/615) 430F/FR 36 A WG (.006) stainless steel (s/s) wire

equals 60 micro ohms per centimeter; Primary Coil (622) 22 A WG (.028) copper wire equals 5.1933 ohms per pound weight; Secondary Pickup Coil (623) 35 A WG (.007) copper wire equals 13K ohms per pound weight. "Pyre-ML" trade name "Himol" polymer coating-material is used to impart thermal and mechanical resistance to the stainless steel (s/s) wire (614/615) coating; both magnet wire sizes (622/623) uses solderable Nysol (Polyurethane Nylon Jacket) insulation enamel coating as a electrical shield-material ... all dielectric coatings having an effective 3KV per mil dielectric value and formulated specifically to endure automotive temperature range from -40° to 155° C.

Inductance Reactance (Rs - Cd - FL)

Inductance Reactance occurs when resistance (Rs), capacitance (Cd), and Inductance (FL) interacts together during D.C. Pulsing (49a xxx 49n), as schematically depicted in (690) of Figure (7-8).

Inductance Reactance not only increases voltage across water-capacitor (ER) beyond applied Voltage Potential (626) of Figure (7-7) but, also, establishes "Impedance Field" (FL) across Inductors (LI-L2) of Figure (7-6) which acts and performs as Resonant Charging Chokes (614/615) of Figure (7-1) once placed on opposite side of capacitor (ER) forming Resonant voltage Effect Circuit (670) of Figure (7-6), as illustrated in (620) of Figure (7-1) as to (690) of Figure (7-8). Both Inductors (LI/L2) are Bifilar wound in equal length to optimize the electromagnetic field strength (FL) in equal electromagnetic intensity ($FLI = FL2$) to encourage and promote "Electron Bounce" phenomenon (700) of Figure (7-9) while adjusting (programmable pulse wave-form) input signal Pulse-Frequency (49a xx 49n) to "tune-in" to the "dielectric property" (Re) of water (85) ... causing amp flow to be reduce to a minimum value while allowing voltage potential (627) of Figure (7-7) to go toward infinity if the electronic components would allow it to happen, as graphically illustrated in (750) of Figure (7-14). Inductance Field (L1-FL1) performs "Capacitance Charging Effect" (628); while, at the same time, Inductor Field (L2- FL2) restricts electron movement through VIC Impedance Network Circuit (620) of Figure (7-1) since Inductance Field (FL2) locks onto Electrons Magnetic Field (647) of Figure (5-9) to block the movement of electron flow toward Positive Voltage Potential (66) ... thereby preventing and inhibiting electron-flow to pass through or arc-over capacitor water-gap (Cp) of Figure (7-8) such electron blocking action is herein called "Electron Inhibiting Effect" (631), as denoted in (670) of Figure (7-6) as to (750) of Figure (7-14). At elevated.or higher amplitude voltage levels (xxx Ve xxx Vf xxx Vn), primary electromagnetic coupling field (Rp) of Figure (7-8) transmitted by

way of Inductance Pulsing-Core (190) of Figure (3-23) as to VIC Coil Assembly (580) of Figure (6-1) enters into and passes through both Inductors (L1/L2) simultaneously and offers not only further electron-flow restriction (Rp 1/Rp2) to both Inductor Chokes (56/62) but automatically increases voltage potential (xxx V g xxx Vh xxx Vn) of opposite voltage intensity of equal magnitude (66/67) across Resonant Cavity (140 -170) ... overcoming any potential loss of pulse signal due to resistive interaction (Rs1/Rs2) of either or both Inductor Cores (L1/L2) wire-material to the formation of Inductance Fields (FL1/FL2) during reoccurring pulse on-time (T1a xxx T1n). Electron Inhibiting Effect (631) in direct relationship to Voltage Enhancement Effect (528) is accomplished since stainless steel 430F/FR wire-material is "Electromagnetic Inductive" to incoming electromagnetic flux-lines (71a xxx 71n) (Rp) without (s/s) inductor-wire-coil (L1/L2) becoming permanently magnetized ... paralleling and performing the same electromagnetic characteristic of copper wire when it comes to magnetic field reformation (Rp - Rp 1 - Rp2) of Figure (7-8), as further illustrated in electromagnetic coupling fields (71 - 511 - 512) of Figure (6-1) that encourages, brings-on, and perform Voltage Inducement Process (580) of Figure (6-1) as to (620) of Figure (7-1) without amp "influxing" (inhibiting amp flow) between Positive Voltage Potential (66) and Negative Voltage Potential (67) electtically applied across Resonant Cavities (140 -170).

In-Line Circuit Components

Lengthening Inductor (L1/L2) lengths applies an even higher Voltage Potential (66/67) across Resonant Capacitor (140 -170) (ER) since Inductance Reactance "Stores" Energy and, is expressed by

(Eq 19)

$$W_a = \frac{L I^2}{Z}$$

Where,

(Wa) is the energy in Joules (Watt-seconds); (L) is the Inductance in Henries; and (I) is the current in amperes.

Inductance Reactance directly determines "Stored" Energy (Wa) Which is controlled by input Voltage Potential attenuated or varied by way of Voltage Amplitude (Vo xxx Va xxx V b - Vf xxx Vg xxx Vn) of Figure (7-13) and/or Gated Pulse-Frequency (49a xxx 49n - T3 - 49a xxx 49n), or both.

Inductance Reactance performs several functions simultaneously or to given stimuli: increases applied voltage amplitude (Vo - Vn), doubles input frequency (64a * 64b) when 50% Duty Cycle Pulse (T1 = T2) is inputted, effectuates "Step Charging Effect" (680) of Figure (7-7) when Pulse off-time (T2) is less than Pulse on-time (T1) ... determining voltage swing from highest voltage level (Vn) to volts switch-off point (Vff), and establishing Impedance (FL) which minimizes heat loss of electrical input power (49) by impairing electron movement.

Inductor (L1) acts and performs in like manner to Inductor (L2) since both Inductor (L1/L2) are physically the same size and shape.

Thermal Explosive Energy-Yield (gtnt)(16a xxx 16n) instantly produced from water (85) is determined by Voltage Amplitude (xxx Vn), Duty Cycle of Pulse Train (T1 - T2a xxx T1 - T2n), Gated Pulse-Frequency of applied Voltage Potential (49a xxx 49n - T3 - 49a xxx 49n), Inductor (L1/L2) length, Secondary Pickup Coil (523) Length (FL3a xxx FL3n), dielectric gap-spacing (Cp), or any combination thereof.

Multi-layer Coil

Inductance of a multilayer coil of rectangular cross section can be computed by below formula when optimizing maximum distributed capacitance (Cda xxx Coo) and distributed inductance (Dla xxx Dln) of Figure (7-3) to intensify Inductance Field Strength (FLa xxx Fln) to function as a voltage multiplier in switch-off conditions (612a xxx 612n), as illustrated in (710) of .. Figure (7-10) as to VIC Coil Assembly (580) of Figure (6-1) and, is expressed:

(Eq 20)

$$L = \frac{0.8 (N \times A)^2}{6A + 9B + 10C} \quad \text{Bobbin Cavity}$$

Where,

(L) is the inductance in microhenries, (N) is the number of turns, (A) is the mean radius in inches, (B) is the length of the coil in inches, (C) is the depth of the coil in inches.

Taper Resonant Capacitor (ERt)

Capacitor (ER) is automatically formed when dielectric liquid of water (Re) is placed between Electrical Conducting Plates (EIIIE2) of Figure (1-1) page (1-13) (Memo WFC 420).

Stainless steel T304 material is used to form Electrical Voltage-Plates (EIIIE2) which do "not" chemically interact (chemically inert) (Lab tested less than .0001/year decomposition rate) with liberated water gases (hydrogen _86, oxygen _87, and non-combustible gases **W** being exposed to an high intensity voltage pulse-field (64a xxx 64n) with negligible amp flow. Electrical Plates herein called "Excitor" Plates or Voltage Zones (E1/E2) can take-on different configuration of shapes to maximize Dynamic Voltage Potential (600) of Figure (6-3) for different application of usage: (35a) Traveling Constant Electrical Voltage Wave by way of linear cylindrical resonant cavity (Tubular Cavity 730A), (35b) Traveling Compressional (concentrating electrical intensity) Electrical Voltage Wave by way of taper cylindrical resonant cavity (730B), (35c) Traveling Expanding Electrical Voltage wave by way of non-linear cylindrical resonant cavity (730C) ... or any voltage surface combination thereof ... each resonant cavity design acting and functioning as a Voltage Wave-guide (570) and gap-size (35) sufficient enough to allow the "Quenching Effect" to take place, as illustrated in (730) of Figure (7-12) as to (370) of Figure (3-40).

The dielectric property of water (being 78.54 ohms @ 25° C) permits the storage of "Electrical Charge" when a potential voltage difference exists between Electrical Voltage-Plates (EIIIE2) as to (E9IEI0).

Capacitance (Cp) of Figure (7-6) as to (690) of Figure (7-8) is determined by the surface area (A) of Electrical Voltage-Plates (E1/E2 - E9/E10), the distance (d) between the Electrical Plates (in inches), and the pennittivity (Eo) of the dielectric property of water (85) and, is expressed in the following equation:

(Eq 21)

$$C = \frac{0.2249 e A}{d Eo} \text{ Picofarads}$$

Where,

(Eo) is Free-Space Permittivity of Water established by VIC Circuit (690) of Figure (7-8) ability to restrict amp flow, (e/Eo) Ratio is the Dielectric Constant of Water, (A) is the surface Area of Resonant Cavity and, is expressed in the below equation:

(Eq 22)

$$\text{area (A) } = \frac{h}{2} (a + b) \text{ Taper Resonant Cavity}$$

Where,

(h) is longitudinal length of tapered resonant cavity, (a) being exit pan circumference surface point (E9d) of Figure (6-2), (b) being cylindrical circumference surface point (E9a) of Figure (6-2) where tapered surface starts, (a) (b) circumference surface points (E9a)(E9d) respectively determined by below expressed equation: (see diagram 720 of Figure 7-11)

(Eq 23)

$$\text{Circumference Surface Point (E9) } = \pi D$$

Where,

(D) is diameter cross section of cylindrical surface at designated point (E9a - E9n), (x) being mathematical constant 3.1416.

Capacitance Reactance

Capacitance Reactance is determined by the insulation resistance (Rs+ Re) and Inductance (LIL2) interacting together during D.C. Pulsing.

Dielectric property of water opposes amp leakage (Re) while another property of water takes-on an "Electrical Charge". Water temperature (Rt) (cool-to-the-touch) keeps (Re) constant since amp flow remains minimal. Plate Inductance (Lc) is Inductance Reactance of Inductor (L1)

and Inductance Reactance of Inductor (L2) in series with Resonant Capacitor (140 -170) of Figure (7-6) as to (690) of Figure (7-8).

In terms of Component Reactance, Inductors (L2) should always be larger than Capacitor (ER) of Figure (7-2) in order to maximize amp restriction to enhance "Voltage Deflection" (SS' - 617a xxx 617n - RR') of Figure (7-4) and, is expressed by :

(Eq 24)

$$Z = X_L - X_C$$

Whereas,

Capacitor (ER) should remain relatively small due to the dielectric value of water to obtain maximum Thermal Explosive Energy-Yield (16a xxx 16n) of Figure (4-5) and subsequently establishing Quenching Circuit (370) of Figure (3-40) to prevent gas ignition inside traveling voltage wave-guide (590) of Figure (6-2) as to (730) of Figure (7-12) ... to bring-on and trigger Hydrogen Fracturing Process (390) of Figure (3-42) once liberated and expanding water gases (100) of Figure (4-8) passes beyond exit port (E9d) ... activating Voltage Ignition Process (90) of Figure (5-5) ... utilizing Dynamic Voltage Potential (600) of Figure (6-3) of opposite electrical stress (SS' - 617 - RR') to cause thermal atomic agitation (90) of Figure (4-7) (kinetic heat by atomic motion) which, when occurring at gas exit port (32) of Figure (4-5), spark-ignites expanding water gas-fuel (45/46/47) of Figure (4-5) during water inject cycle (70) of Figure (4-5) ... releasing thermal explosive energy (gtnt) (16) under control state.

Circuit Resistance

Total VIC "Circuit Resistance" to D.C. current flow is expressed and determined by:

(Eq 9)

$$Z = R_I + Z_2 + Z_3 + R_E$$

Where,

(R_I) is the resistive value of Secondary Pickup Coil (52) of Figure (7-8) plus Magnetic Field strength of primary coupling field (71) in direct relationship to inductance field strength (R_p) which is determined by the number of turns of wire that make up secondary coil-wrap (52), (Z₂) is determined by inductance field strength (FL1) and resistive value (RS1) (typically 11.6 KQ) of

stainless steel (s/s) wire-coil (56) (LI) when being exposed to external magnetic coupling field strength (Rp), (Z3) is determined by inductance field strength (FL2) and resistive value (RS2) (typically 11.6KQ) of stainless steel (sls) wire-coil (62)(L2) when being exposed to the same external magnetic coupling field strength (Rp) ... each choke-coil (LIL2) being of the same impedance value since both coil-wraps (56/62) are Bifilar wound together onto a single spool-bobbin, (Re) is the dielectric property of water and it's resistive value is typically (78.54 Q) since "rain water" (85f) contains less than 20ppm of any type of contaminates due to Water Evaporation Process (530) of Figure (5-6). (see VIC Matrix Circuit 690 of Figure 7-8 as to Water Chan (760) of Figure (7-15), once again)

Transformer Action

Inductance Core (53) of Figure (6-1) composed of "Grain Oriented" Electrical Steel laminations step up applied Voltage (49) when Magnetic Field Coupling (71) of Figure (7-8) cross over to Secondary Pickup Coil-winding (52) which has more turns of wire than Primary Coil-winding (26) by way of "Eddy" currents that induces magnetic flux lines of forces (71a xxx 71n) emanating away from magnetic core material (53) and caused by Primary Coil (26) being electrically energized during pulsing operations (T1a xx T1n), as illustrated in (690) of Figure (7-8). Magnetic Induction (71a - 71n) is determined by Inductance Permeability (μL) of core material (53) along with VIC circuit geometry ability to step up Voltage Potential ($V_o - V_n$) by way of "Transformer Action", and is expressed in the following equations:

(Eq 25)

$$\frac{E_p}{E_s} = \frac{N_p}{N_s} \quad \text{and} \quad \frac{E_p}{E_s} = \frac{I_s}{I_p}$$

Where,

(E_p) is voltage induced in Primary Coil (26), (E_s) is Voltage induced in Secondary Coil (52), (N_p) is the number of turns of wire that make up Primary Coil-Wrap (504) of Figure (6-1), (N_s) is the number of turns of wire that make up Secondary Coil-Wrap (505) of Figure (6-1), (I_s) is the established current flow (under load) in Secondary Coil-Winding (52) , (I_p) is the amount of current flow in the Primary Coil-Winding (26) when electrically "energized" during pulsing operations (49a xxx 49n - T3 - 49a xxx 49a).

The turns ratio of the VIC Transformer (26/52) is determined by the following equation:

(Eq 26)

$$T = \frac{N_s}{N_p}$$

Where,

(Ns) is the number of turns of wire for each bobbin cavity (505) of Figure (6-1) as to (710) of Figure (7-10) that are electrically connected in series arrangement (505a xxx 505n) to form Secondary Coil-Wrap (52), (Np) is the number of turns of the primary Coil (26) wire-wrapped about spool cavity (504) ... each bobbin cavity adhering to equation (Eq 20), as illustrated in (710) of Figure (7-10).

The impedance ratio of VIC transformer is determined by:

(Eq 27)

$$Z = T^2$$

Where,

(1'2) is the sum of the magnetic field strength (FL4) of the primary coil (26) and the induced magnetic field (FL3) of the Secondary Pickup Coil (52) during each pulse cycle (TI) in direct relationship to repetitive pulse cycling (T1a xxx T1n) and both magnetic fields (FL31FL4) interacting, and is expressed in the following equation:

(Eq 28)

$$M = \frac{La}{4}$$

Where,

(M) is the mutual inductance expressed in the same units as (La), (La) is the total inductance of Primary coil (26) and Secondary coil (52) with fields aiding.

Coupling Inductance (R_p) between the Primary coil (26) and Secondary Coil (52) is further extrapolated in the following equation:

(Eq 29)

$$L_t = \frac{1}{\frac{1}{L_1 + M} + \frac{1}{L_2 + M}} \quad \text{Transformer}$$

Where,

(L_t) is the total inductance, (L_1) and (L_2) are the inductance of each individual transformer coils (26)(52), (M) is the mutual inductance of each transformer coil (26/52) being in parallel relationship with fields aiding.

Coupling Inductance (R_{p1}) and (R_{p2}) in (690) of Figure (7-8) is further expressed in the following equation:

(Eq 30)

$$L_{tcc} = L_1 + L_2 + 2M \quad \text{Choke Coils}$$

Where,

(L_{tcc}) is the total inductance of Choke Coils (FL1 - FL2), (L_1) and (L_2) are the inductance of each individual choke coil (56)(62) in series with Secondary Coil (52) Electrical Voltage Potential (700) of Figure (7-9) and being exposed to the same Voltage Transformer (26 - 53 - 52) magnetic field (R_p) with aiding fields, (M) is the mutual inductance of choke coils (L_1/L_2) since Transformer Magnetic Field (R_p) is the excitation External Magnetic Field (R_{p1}/R_{p2}) by way of Unipolar Pulsing Core (53).

VIC Coil Assembly (580) of Figure (6-1) as to (690) of Figure (7-8) in reference to Schematic Circuit (620) of Figure (7-1) is constructed in such a way as to rotate and position Inductor Coils (26 - 52 - 56 - 62) to be of the same electromagnetic polarity orientation, indicator mark (e) ... thus, allowing Inductance Fields (FL1 - FL2 - FL3 - FL4) to be aiding one another during the same sequence of pulse-time (T_1) ... thereby, allowing Inductance Charging Effect (660) of Figure (7-5) and Resonant Voltage Effect (670) of Figure (7-6) to interact with the dielectric properties of water (R_e) to cause and inhibit electron flow (IF) since "electrons" magnetic

field (547) of Figure (5-9) locks onto the electromagnetic fields of each energized choke coils (FL1/FL2) during Voltage Excitation ($V_o - V_n$) which, now, brings on and allows "Electron Bounce Phenomenon" (700) of Figure (7-9) to take place. (See Appendix B Note 1)

Electron Bounce Phenomenon

High Voltage Potential of Difference ($V_o - V_n$) ($SS' - 617 - RR'$) is accomplished when magnetic flux lines of force (71a xx 71) (R_p) emanating away from closed-loop magnetic pulsing core (53) of Figure (190) penetrates Inductance coil-windings (52 - 56 - 62) simultaneously during each and every pulse on-time (T_{1a} xxx T_{1n}) as programmable pulse-train (49a xxx 49n $T_3 - 49a$ xxx 49n) is adjusted to "Tune - in" to the dielectric property of Water (R_e) causing mutual inductance (μ_1) (see equations Eq 28 thru Eq 30) to transform Distributed Capacitance (C_{da} xxx C_{dn}) of Figure (7-3) of each inductance coils (52 - 56 - 62) into a coherent Voltage Potential ($V_o \bullet \bullet V_n$) equaling the sum of Voltage Potential (V_p) developed across each Pickup Coils ($V_{pT} + V_{p1} + V_{p2}$) ..• producing Dynamic Voltage Potential (600) of Figure (6-3) during repetitive pulsing (49a xxx 49n - $T_3 - 49a$ xxx 49n) ... setting up and performing pulsating Opposite Electrical Attraction Force ($SS' \sim 617 \sim RR' - T_3 - SS' \sim 617 - RR'$) of Figure (7-4) as to Voltage Dynamics (220) of Figure (3-29) ... triggering Hydrogen Fracturing Process (90) of Figure (5.5) as to (100) of Figure (4-8) ... instantly releasing thermal explosive energy (gtnt) (16) from Water (85) on demand, as illustrated in Taper Resonant Cavity (590) of Figure (6-2) as to (70) of Figure (4-5). The resultant Dynamic Voltage Potential of Difference (opposite electrical attraction force) ($SS' - 617 \bullet \bullet RR'$) is in balance phase of equal electrical intensity ($66 = 67$) of opposite polarity (positive electrical voltage potential $_66$ equals negative electrical Voltage potential $\underline{66}$ since the voltage Coefficient of Inductance (FL1/FL2), Voltage Coefficient of Capacitance (C_{d1}/C_{d2}), and voltage Coefficient of Resistance (R_{s1}/R_{s2}) across choke coils (L_1/L_2) are the same values ... allowing, Voltage Bounce Phenomenon (700) of Figure (7-9) to be preformed.

Magnetic Field Coupling (71) of Figure (7-9) entering into and passing through Secondary Coil-winding (52) of Figure (7-8) causes and produces copper ions (643a xxx 643n) (Positive Charged atoms 542a xxx 542n having missing electrons) when moving external electromagnetic field strength (71a xxx 71n) is sufficient enough to dislodge electromagnetically charged electrons (64Ia xxx 64In) from copper atoms making up copper wire material (52). Collectively, the resultant positive electrical charged copper ions (642a xxx 642n) added together produces Positive Voltage Potential (629) being electrically applied to choke-coil (56); whereas, the "Liberated" negative electrical charged electrons (64Ia xxx 64In) added together provides Negative Voltage

Potential (631) to the opposite end of Secondary Wire (52) being electrically connected to choke coil (62). Once Secondary Coil-winding (52) is de-energized by the removal (collapsing magnetic field during pulse off-time T_2 of external Magnetic Field (71), the dislodged electrons (641a xx 641n) return to positive charged copper ions (642a xx 642n) ... terminating and switching off opposite voltage potential (629 - 631) when positive electrical state of the copper atoms changes back to net electrical charge of zero. Sustaining and maintaining the resultant induced Voltage Potential ($V_o - V_n$) without "Electron Discharged" (inhibiting electron flow) through Choke Coil (62) while, at the same time, inhibiting (preventing) any additional or other electrons from entering into Secondary copper wire-zone (52) by way of Choke Coil (56) is herein called "Electron Bounce Phenomenon" (EbP), as illustrated in (700) of Figure (7-9).

Electrically Interlinked serially together, Electron Bounce Phenomenon (EbP) , Voltage Coefficient of Inductance (F_{I1}/F_{I2}), Voltage Coefficient of Capacitance (C_{d1}/C_{d2}), Voltage Coefficient of Resistance (R_{s1}/R_{s2}), and dielectric Coefficient of Water resistance (R_e) allows Voltage Potential ($V_o - V_n$) of opposite electrical polarity to perform work ($SS' - 617 - RR'$) without amp influxing " thus, not allowing the introduction of electron flow into Hydrogen Fracturing Process (90) of Figure (5-5) during Voltage Stimulation ($SS' - 617 - RR'$) ... causing "electron clustering" (641a xxx 641n) to take place within Copper Wire Zone (52) during pulse on-time (T_1) ... inhibiting "electron flow" to maintain opposite voltage potential ($66/E_9 - 67/E_{10}$) across Resonant Water Gap (616) during the process of converting water-fuel (85) into instant thermal explosive energy (gtnt) ... therefore, producing a physical force-yield (F_y) during gas-ignition (70) of Figure (4-5) which is directly related to the liquid volume of water (85) per injection cycle and applied Resonant Voltage Intensity ($Y_o - V_n$), as illustrated in (590) of Figure (6-2) as to (90) of Figure (5-5) .

. Of course, in practical terms of component interaction, a minute amount of amp leakage is present and does occur due to Electronic Component Limitations but is negligible as to the overall performance of the Hydrogen Fracturing Process (590) of Figure (6-2) when being subjected to either one of traveling Electrical Voltage Wave-forms (730a - b - c) of Figure (7-12), see Voltage Graph (750) of Figure (7-14) once again.

Voltage Amplitude Switch-Off

Voltage levels of variance (V_a xxx V_n) is achieved by simply switching-in or switching-out the member of Secondary Coil-cavities (505a xx 505n) (see 740 of Figure 7-13) in direct

relationship to Taper Resonant Voltage surfaces (E9/10) of Figure (6-2) which acts and performs as a "Voltage Amplifier" when Compressional Wave-form (B) of Figure (7-12) is intensified at Exit Port (32) of Figure (6-2). Switching the member of Secondary Coil-Array (505a xxx 505n) maximizes electrical power transfer from Primary Coil (26) to Secondary Coil (52) by keeping Voltage Amplitude of Pulse-train (49a xx 49n - T3 - 49a xxx 49n) constant.

Mode of Operability

The established "mode-of-operability" of VIC Coil Assembly (580) of Figure (6-1), now, allows Voltage Potential (Vn) of opposite voltage polarity (66/SS' - 67/RR') to increase and be attenuated up to and beyond 20 Kilovolts while inhibiting and restricting amp leakage in the milliamperes range ... establishing operational parameter of utilizing Opposite Electrical Attraction Force (SS' - RR') of high voltage intensity (Vn) to instantly release thermal explosive energy (gtnt) from natural water. Voltage Compressional Wave-form (35b) and Expanding Voltage Waveform (35c) increases the intensity of applied pulsating opposite electrical attraction force (55' -RR'a xxx SS' - RR'n) even further during each new pulse-cycle (T2 next T2) across watergap (616) ... increasing Thermal Explosive Energy-yield (gtnt) to higher energy-levels (gtnta xxx gtntn) beyond applied excitation voltage (Vn) by simply altering Voltage Surfaces (35b/35c) as in reference to Linear Voltage Surfaces (35a), as illustrated in (730) of Figure (7-12). Pulse Off-time (T2) of Figure (7-8) as to (620) of Figure (7-1) is adjusted to compensate for the rise and fall of magnetic coupling field (71) to produce applied Unipolar Wave-forms (64a xxx 64n) entering into Wave-guides (35a/35b/35c). Less water contaminants nets even higher energy-yield (gtnta xxx 85a - 85h xxx gtntn), as illustrated in Water Chart (760) of Figure (7-15). In terms of thermal explosive energy-yield (gtnt) under dynamic pressure of compression approximately 7.4 (μl) microliter of a liquid-volume of a water droplet per injection cycle is all that ~s required to run the Dune Buggy 1600cc 50hp VW I.C. engine at 65 m.p.h. on the open road; whereas, a typical 325 hp diesel I.C. truck-engine would require about 48.1 (μl) microliters of a water droplet per injection cycle to accomplish the same open road performance. (see WFC Water vs Gasoline Energy Content Equations (memo WFC 429).

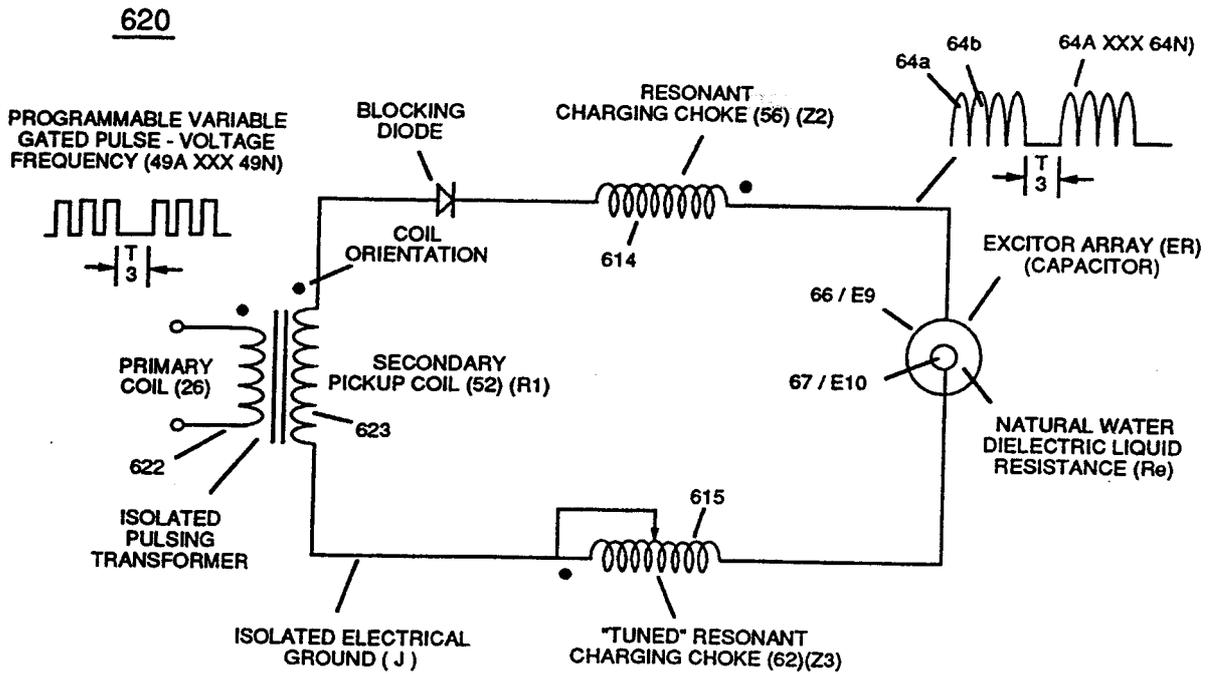


FIGURE 7-1: VIC IMPEDANCE NETWORK

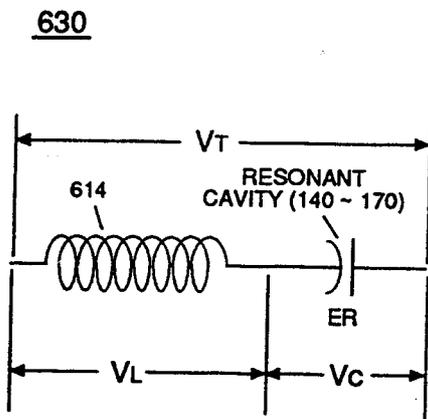


FIGURE 7-2: LC CIRCUIT

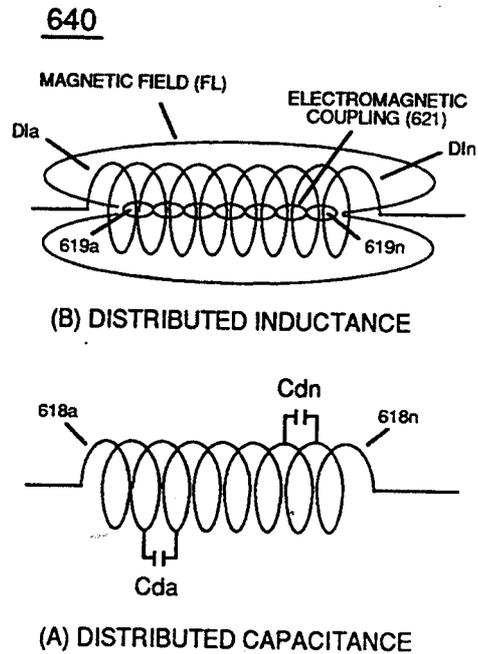


FIGURE 7-3: COIL INTERACTION

650

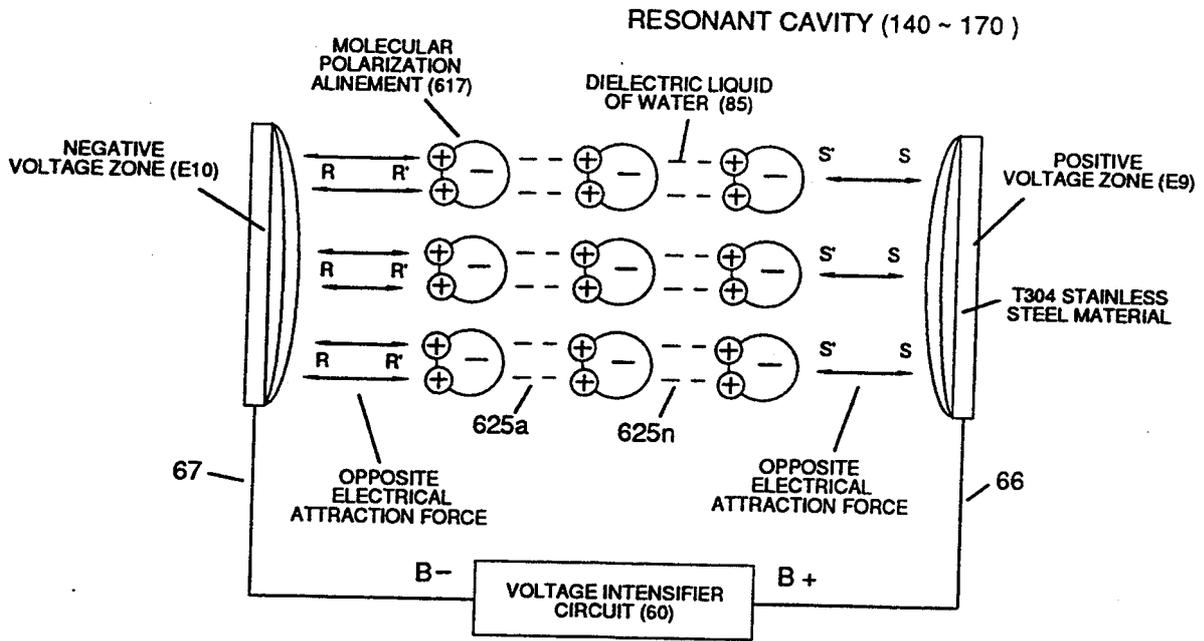


FIGURE 7-4: ELECTRICAL CHARGING EFFECT

660

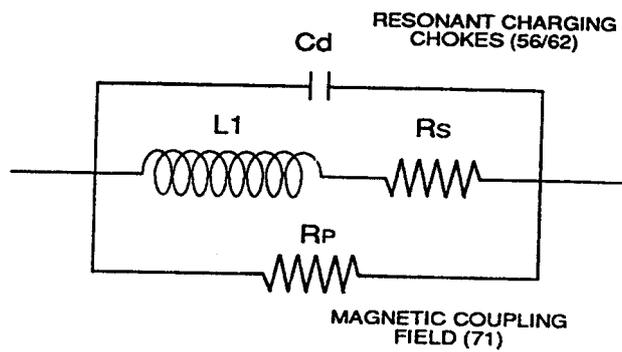


FIGURE 7-5: INDUCTANCE CHARGING EFFECT.

670

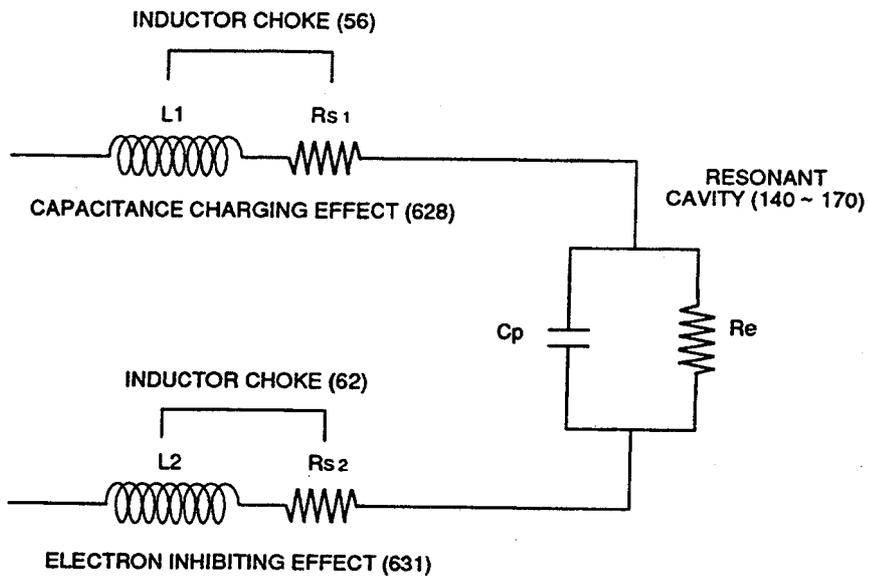


FIGURE 7-6: RESONANT VOLTAGE EFFECT

680

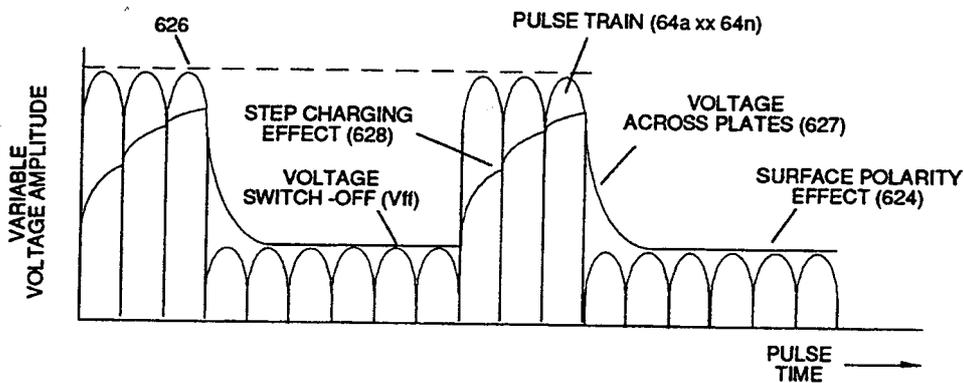


FIGURE 7-7: VOLTAGE CHARGING EFFECT

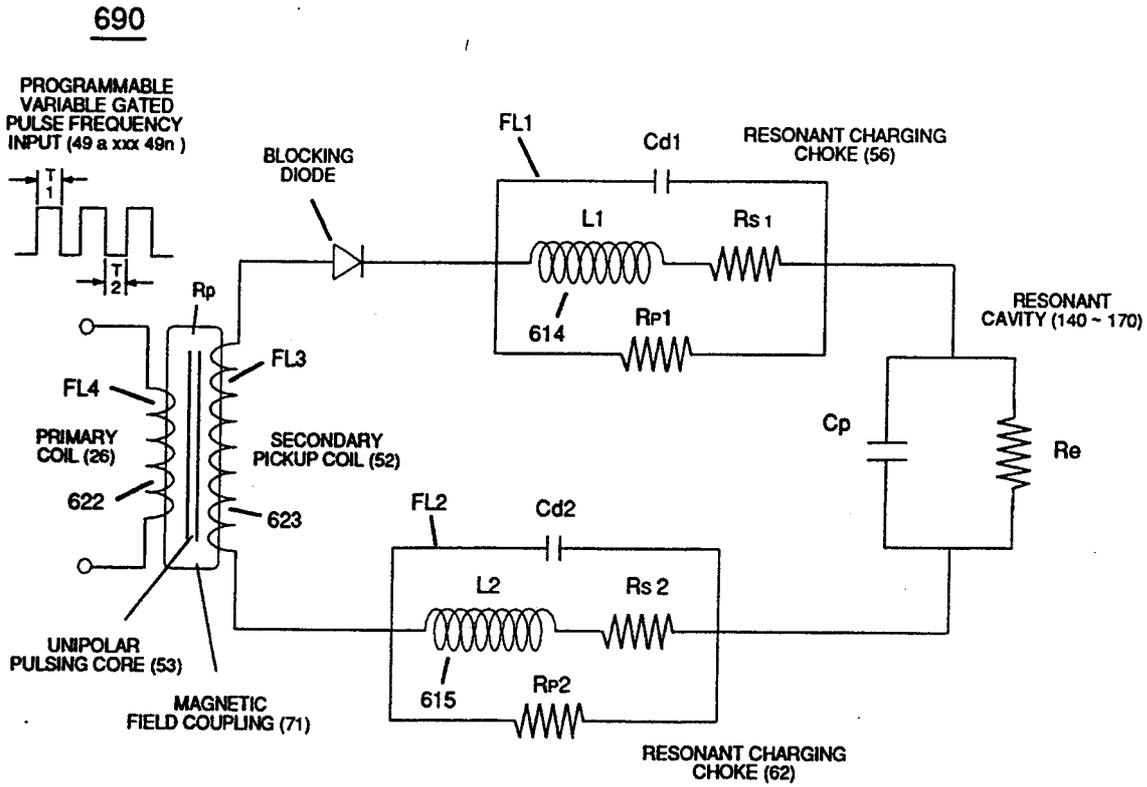


FIGURE 7-8: VIC MATRIX CIRCUIT

700

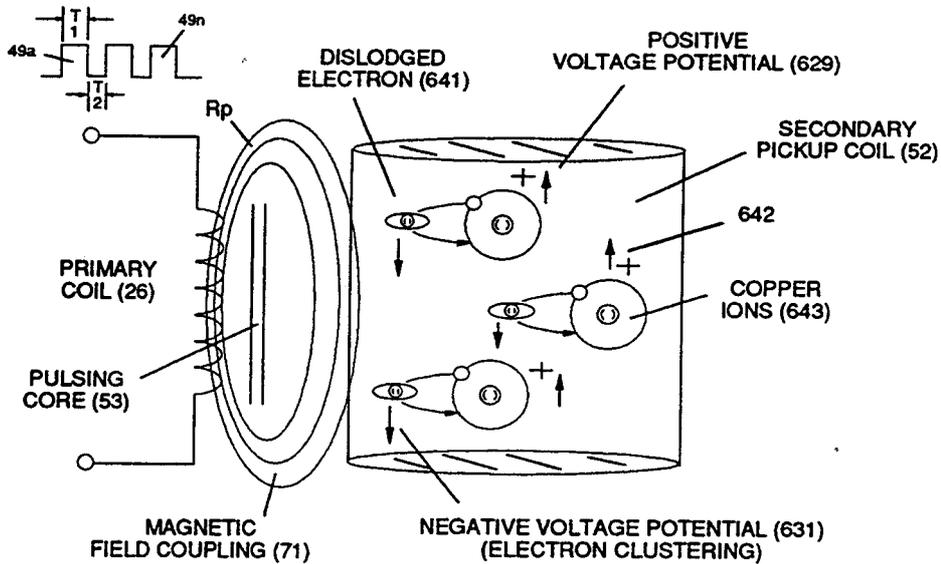


FIGURE 7-9: ELECTRON BOUNCE PHENOMENON (EbP)

710

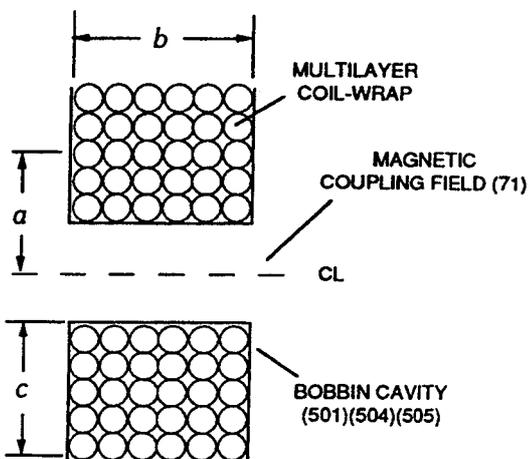


FIGURE 7-10: VOLTAGE STEPPING COILS

720

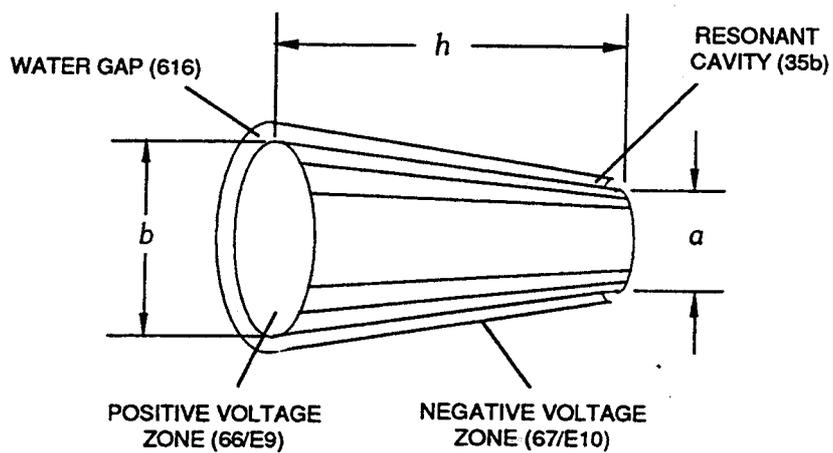
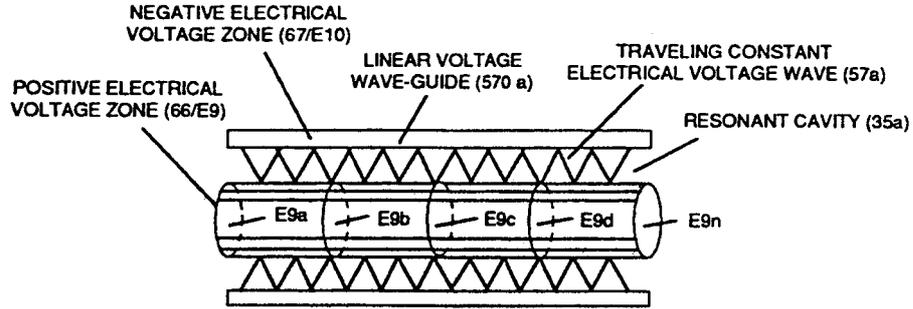
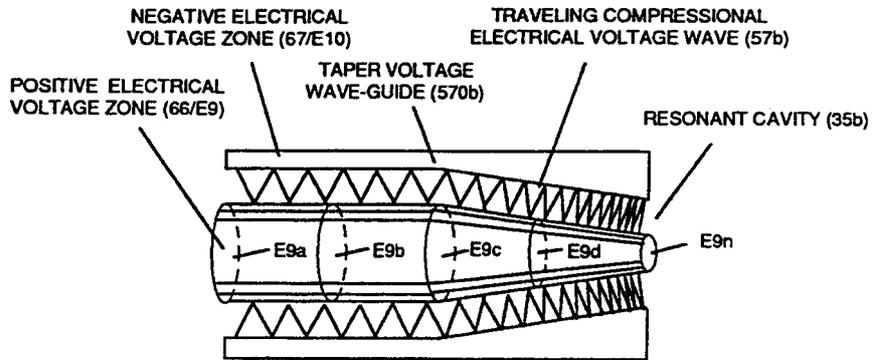


FIGURE 7-11: TAPERED VOLTAGE WAVE-GUIDE

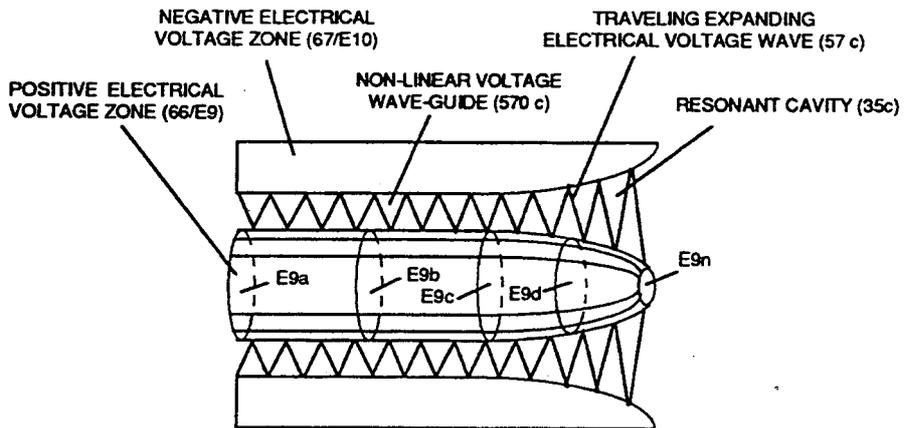
730



(A) LINEAR CYLINDRICAL RESONANT CAVITY



(B) TAPER CYLINDRICAL RESONANT CAVITY



(C) NON-LINEAR CYLINDRICAL RESONANT CAVITY

FIGURE 7-12: RESONANT CAVITY ELECTRICAL VOLTAGE WAVE

740

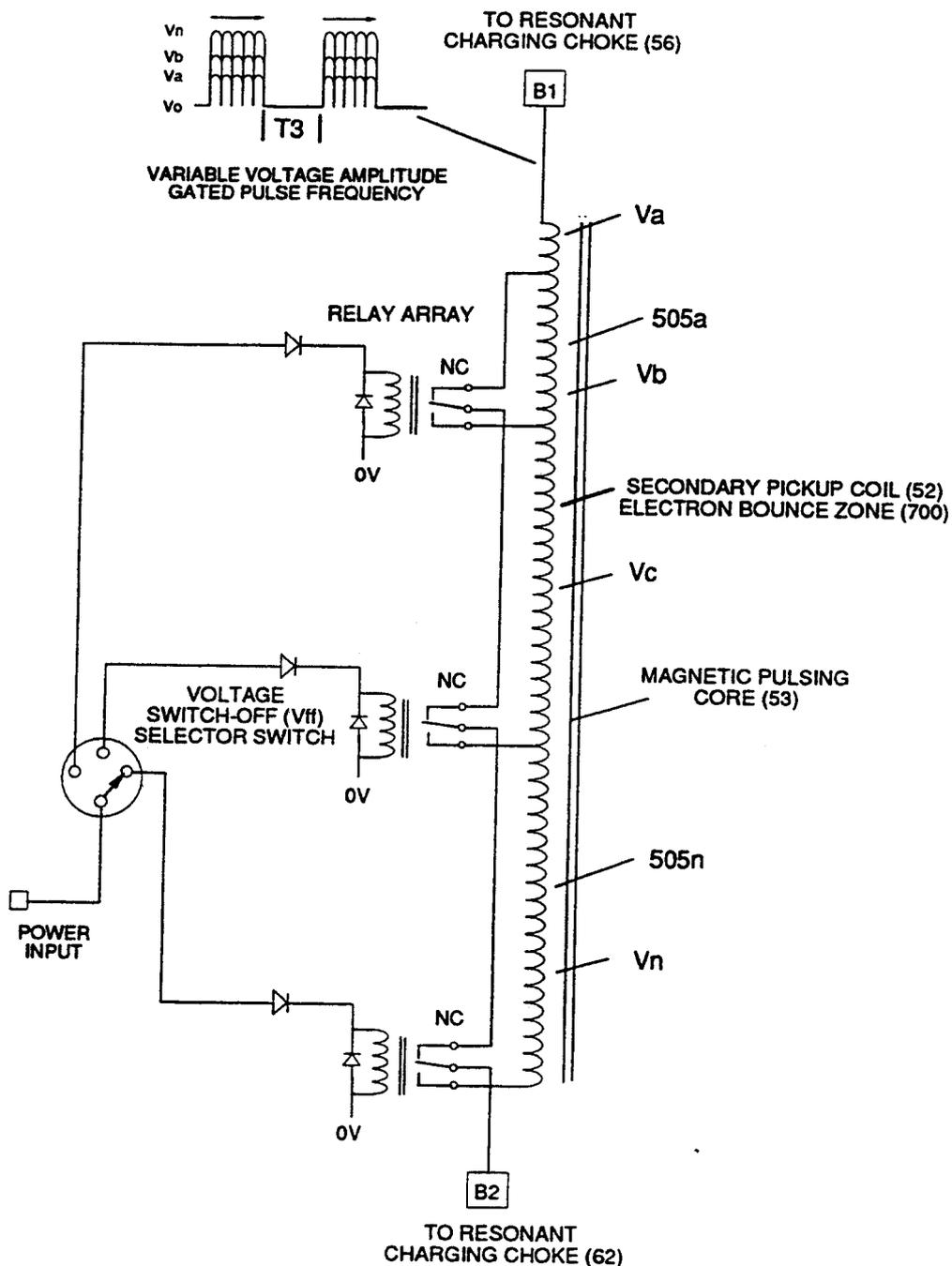


FIGURE 7-13: VIC SECONDARY SWITCH-OFF COIL-ARRAY

750

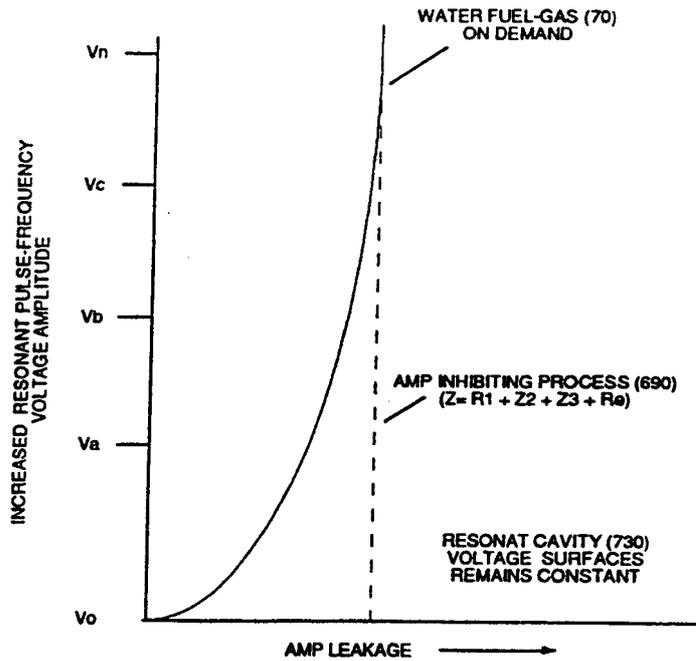


FIGURE 7-14: RESONANT CAVITY WATER-FUEL INJECTION

760

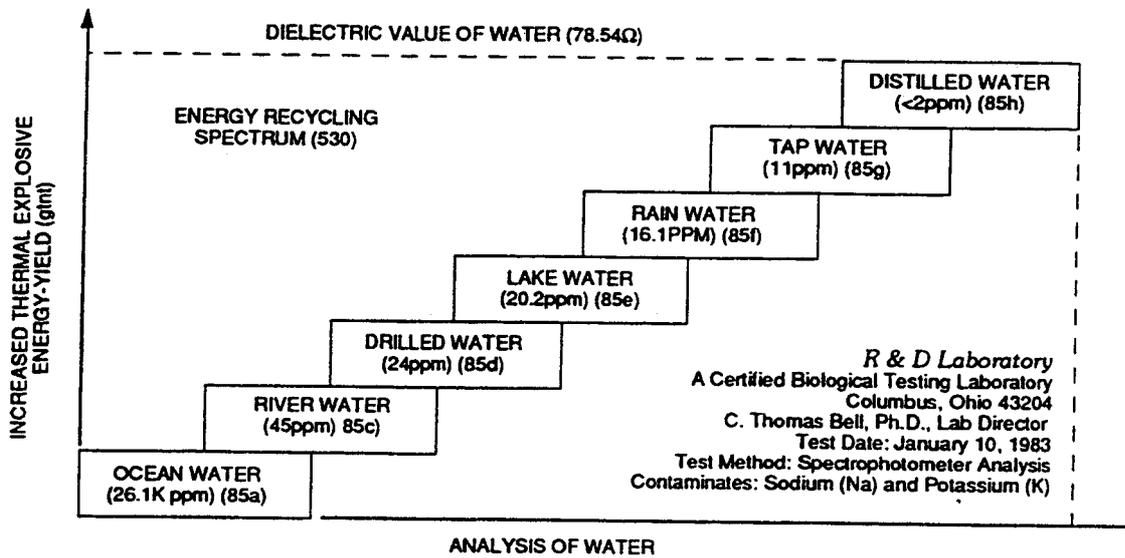


FIGURE 7-15: THERMAL EXPLOSIVE-ENERGY OF WATER